# Thermomechanical Topology Optimization of Shape-Memory Alloy Structures Using a Transient Bilevel Adjoint Method



Ziliang Kang, \*Kai A. James

Department of Aerospace Engineering University of Illinois at Urbana-Champaign

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# Shape-Memory Alloys: An Overview

- Shape change in response to thermal loads ۲
- Continuous "fluid" motion with infinite • degrees of freedom
- **Bio-inspired design** •
- Programmable motion



The BioRobotics Institute/Scuola Superiore Sant'Anna 2019

Key contributions: - Novel topology optimization formulation - Bi-level adjoint sensitivity formulation

## Phase Transformation

- Inelastic stress and strain response due to phase transformation
- Triggered by latent heat exchange
- Transformation between Martensite and Austenite phases



Two-way shape-memory effect

Lagoudas 2008



Superelasticity

Lagoudas, DC. Shape Memory Alloys: Modeling and Engineering Applications. Berlin, Germany: Springer; 2008.

Seo, Junwon, Young Chan Kim, and Jong Wan Hu. "Pilot study for investigating the cyclic behavior of slit damper systems with recentering shape memory alloy (SMA) bending bars used for seismic restrainers." Applied Sciences 5.3 (2015): 187-208.

#### Constitutive Model

• Additive decomposition of small strains

$$\begin{split} \varepsilon &= \varepsilon^{e}(\sigma) + \varepsilon^{t}(\sigma, T, \xi) + \varepsilon^{th}(T) \\ S &= S^{A} + \xi(S^{M} - S^{A}) = S^{A} + \xi \Delta S \\ \alpha &= \alpha^{A} = \alpha^{M} \\ c &= c^{A} = c^{M} \\ \dot{\varepsilon}^{t} &= \mathbf{\Lambda} \dot{\xi} \\ \dot{\mathbf{\Lambda}} &= \begin{cases} \frac{3}{2}H \frac{\sigma_{s}}{\sigma_{s}^{eff}} & \dot{\xi} > 0 \\ H \frac{\varepsilon_{t-r}}{\varepsilon_{t-r}^{eff}} & \dot{\xi} < 0 \end{cases} \\ \mathrm{Transformation tensor} \\ \mathrm{d}\sigma &= \mathfrak{L} : \mathrm{d}\varepsilon \end{split}$$

$$\boldsymbol{\mathfrak{L}} = \begin{cases} \boldsymbol{S}^{-1} - \frac{\boldsymbol{S}^{-1}:\partial_{\boldsymbol{\sigma}} \Phi \otimes \boldsymbol{S}^{-1}:\partial_{\boldsymbol{\sigma}} \Phi}{\partial_{\boldsymbol{\sigma}} \Phi:\boldsymbol{S}^{-1}:\partial_{\boldsymbol{\sigma}} \Phi - \partial_{\boldsymbol{\xi}} \Phi} & \dot{\boldsymbol{\xi}} > 0\\ \boldsymbol{S}^{-1} - \frac{\boldsymbol{S}^{-1}:\partial_{\boldsymbol{\sigma}} \Phi \otimes \boldsymbol{S}^{-1}:\partial_{\boldsymbol{\sigma}} \Phi}{\partial_{\boldsymbol{\sigma}} \Phi:\boldsymbol{S}^{-1}:\partial_{\boldsymbol{\sigma}} \Phi + \partial_{\boldsymbol{\xi}} \Phi} & \dot{\boldsymbol{\xi}} < 0 \end{cases}$$

#### Finite Element Implementation

Global level :

$$\boldsymbol{R}_{n+1} = \bigwedge_{\mathrm{el}} (\sum_{\mathrm{G}^{\mathrm{d}}} (w \boldsymbol{B}_{\mathrm{G}^{\mathrm{d}}}^{\mathrm{T}} \boldsymbol{\sigma}_{\mathrm{G}^{\mathrm{d}}, n+1}) - \sum_{\mathrm{G}^{\mathrm{f}}} (\varpi \boldsymbol{N}_{\mathrm{G}^{\mathrm{f}}} \boldsymbol{p}_{\mathrm{G}^{\mathrm{f}}, n+1})) = 0$$

Local level :

$$\begin{split} \dot{\xi} \neq 0 : \\ \mathbf{H}_{\xi} &= \Phi(\mathbf{\sigma}_{n+1}, T_{n+1}, \xi_{n+1}) \\ \mathbf{H}_{\varepsilon^{t}} &= \varepsilon_{n}^{t} + \mathbf{\Lambda}(\xi_{n+1} - \xi_{n}) - \varepsilon_{n+1}^{t} \\ H_{S} &= S_{n} + \Delta S(\xi_{n+1} - \xi_{n}) - S_{n+1} \\ \mathbf{H}_{\sigma} &= \mathbf{\sigma}_{n} + \mathbf{S}_{n+1}^{-1} : [\mathbf{B}\mathbf{d}_{n+1} - \mathbf{\alpha}(T_{n+1} - T_{0}) - \varepsilon_{n+1}^{t}] \\ &- \mathbf{S}_{n}^{-1} : [\mathbf{B}\mathbf{d}_{n} - \mathbf{\alpha}(T_{n} - T_{0}) - \varepsilon_{n}^{t}] - \mathbf{\sigma}_{n+1} \\ \dot{\xi} &= 0 : \end{split}$$

$$\boldsymbol{H}_{n+1} = \boldsymbol{\sigma}_n + \boldsymbol{S}^{-1} : \left[ (\boldsymbol{B}\boldsymbol{d}_{n+1} - \boldsymbol{\alpha}(T_{n+1} - T_0) - \boldsymbol{\varepsilon}^t) - (\boldsymbol{B}\boldsymbol{d}_n - \boldsymbol{\alpha}(T_n - T_0) - \boldsymbol{\varepsilon}^t) \right] - \boldsymbol{\sigma}_{n+1} = 0$$



## **Optimization Problem Formulation**

Two-phase topology optimization:



Two-way shape-memory effect (geometric advantage):

$$f_{obj} = \boldsymbol{L}^{\mathrm{T}} \boldsymbol{d}$$

Superelasticity (mechanical advantage):

$$f_{obj} = \frac{\boldsymbol{F}_{out}}{|\boldsymbol{F}_{in}|} = \frac{\boldsymbol{L}_{out}^{\mathrm{T}}\boldsymbol{F}}{|\boldsymbol{F}_{in}|}$$

Material interpolation scheme:

$$E^{\text{eff}} = r^p E^*$$
$$dT^{\text{eff}} = r^p dT^*$$
$$V^{\text{eff}} = rV^*$$



#### Adjoint Sensitivity Analysis

$$n = N_{t}: \begin{cases} \boldsymbol{\lambda}_{N_{t}} = \left[\frac{\partial \boldsymbol{R}_{N_{t}}}{\partial \boldsymbol{u}_{N_{t}}} - \bigwedge_{\mathrm{el}} \sum_{\mathrm{G}} \frac{\partial \boldsymbol{R}_{N_{t}}}{\partial \boldsymbol{\nu}_{\mathrm{G},N_{t}}} \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},N_{t}}}{\partial \boldsymbol{\nu}_{\mathrm{G},N_{t}}}\right)^{-1} \frac{\partial \boldsymbol{H}_{\mathrm{G},N_{t}}}{\partial \boldsymbol{u}_{N_{t}}}\right]^{-\mathrm{T}} \\ \cdot \left[\bigwedge_{\mathrm{el}} \sum_{\mathrm{G}} \frac{\partial f_{int}}{\partial \boldsymbol{\nu}_{\mathrm{G},N_{t}}} \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},N_{t}}}{\partial \boldsymbol{\nu}_{\mathrm{G},N_{t}}}\right)^{-1} \frac{\partial \boldsymbol{H}_{\mathrm{G},N_{t}}}{\partial \boldsymbol{u}_{N_{t}}} - \frac{\partial f_{int}}{\partial \boldsymbol{u}_{N_{t}}}\right]^{\mathrm{T}} \\ \gamma_{\mathrm{G},N_{t}} = - \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},N_{t}}}{\partial \boldsymbol{\nu}_{\mathrm{G},N_{t}}}\right)^{-1} \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},N_{t}}}{\partial \boldsymbol{\nu}_{\mathrm{G},N_{t}}}\right)^{-1} \frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{u}_{\mathrm{G},N_{t}}}\right)^{\mathrm{T}}, \forall \mathrm{G} \end{cases}$$

$$n < N_{t}: \begin{cases} \boldsymbol{\lambda}_{n} = \left[\bigwedge_{\mathrm{el}} \sum_{\mathrm{G}} \frac{\partial \boldsymbol{R}_{n}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}} \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}}\right)^{-1} \frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{u}_{n}} - \frac{\partial \boldsymbol{R}_{n}}{\partial \boldsymbol{u}_{n}}\right]^{-\mathrm{T}} \\ \cdot \left\{\lambda_{n+1}^{\mathrm{T}} \left[\frac{\partial \boldsymbol{R}_{n+1}}{\partial \boldsymbol{u}_{n}} - \bigwedge_{\mathrm{el}} \sum_{\mathrm{G}} \frac{\partial \boldsymbol{R}_{n+1}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}} \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}}\right)^{-1} \frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{u}_{\mathrm{G},n}}\right]^{-1} \\ + \bigwedge_{\mathrm{el}} \sum_{\mathrm{G}} \gamma_{\mathrm{G},n+1}^{\mathrm{T}} \left[\frac{\partial \boldsymbol{H}_{\mathrm{G},n+1}}{\partial \boldsymbol{u}_{n}} - \frac{\partial \boldsymbol{H}_{\mathrm{H},1}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}} \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}}\right)^{-1} \frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{u}_{\mathrm{G},n}}\right]^{\mathrm{T}} \\ \gamma_{\mathrm{G},n} = - \left(\frac{\partial \boldsymbol{H}_{\mathrm{G},n}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}}\right)^{-\mathrm{T}} \left(\lambda_{n}^{\mathrm{T}} \frac{\partial \boldsymbol{R}_{n}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}} + \lambda_{n+1}^{\mathrm{T}} \frac{\partial \boldsymbol{R}_{\mathrm{H},1}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}} + \gamma_{\mathrm{G},n+1}^{\mathrm{T}} \frac{\partial \boldsymbol{H}_{\mathrm{G},n+1}}{\partial \boldsymbol{\nu}_{\mathrm{G},n}}\right]^{\mathrm{T}}, \forall \mathrm{G}$$

# Example Problem 1: TWSME

$$\begin{array}{ll} \min & f_{obj} = -\boldsymbol{L}^{\mathrm{T}}\boldsymbol{d} \\ & s.t \quad \boldsymbol{L}^{\mathrm{T}}\tilde{\boldsymbol{d}} \leq 3 \times 10^{-4}\mathrm{m} \\ & V \leq 0.3 \end{array}$$





#### Example Problem 2: Superelasticity



# Summary & Future Work

- Topology optimization/material interpolation scheme
- Path-dependent, transient adjoint formulation
- 2D examples for TWSME and superelasticity
- Future work:

Coupled thermal conductivity (heat diffusion, joule heating)
 3D robotic mechanisms; 4D printing

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# Thank you!

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