

# Multi-material topology optimization of lattice structures using geometry projection

TOP Webinar

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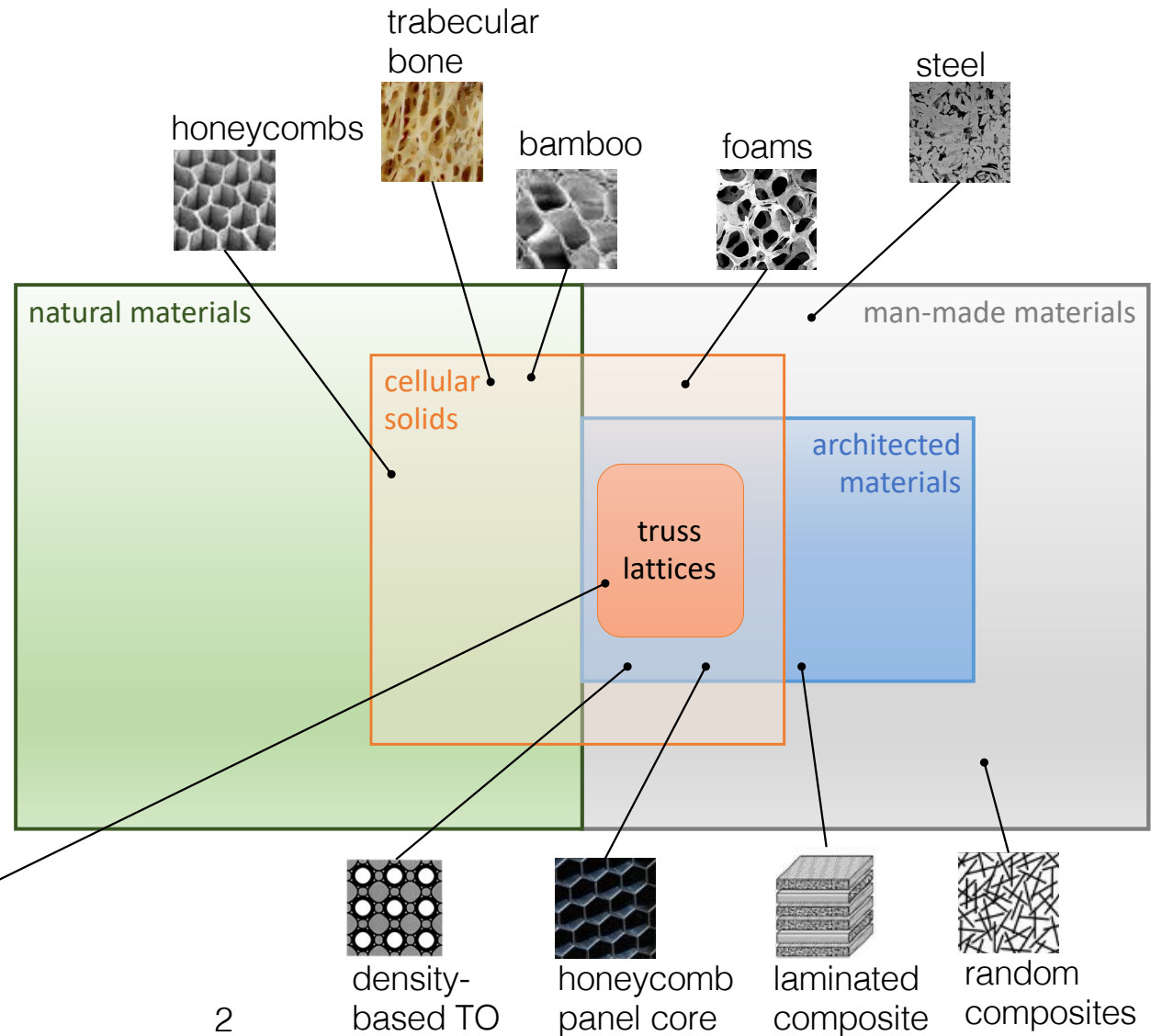
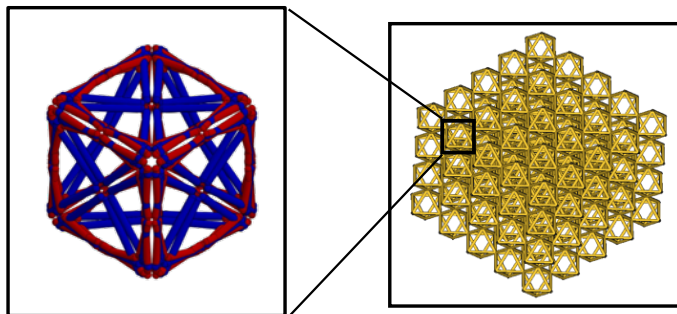
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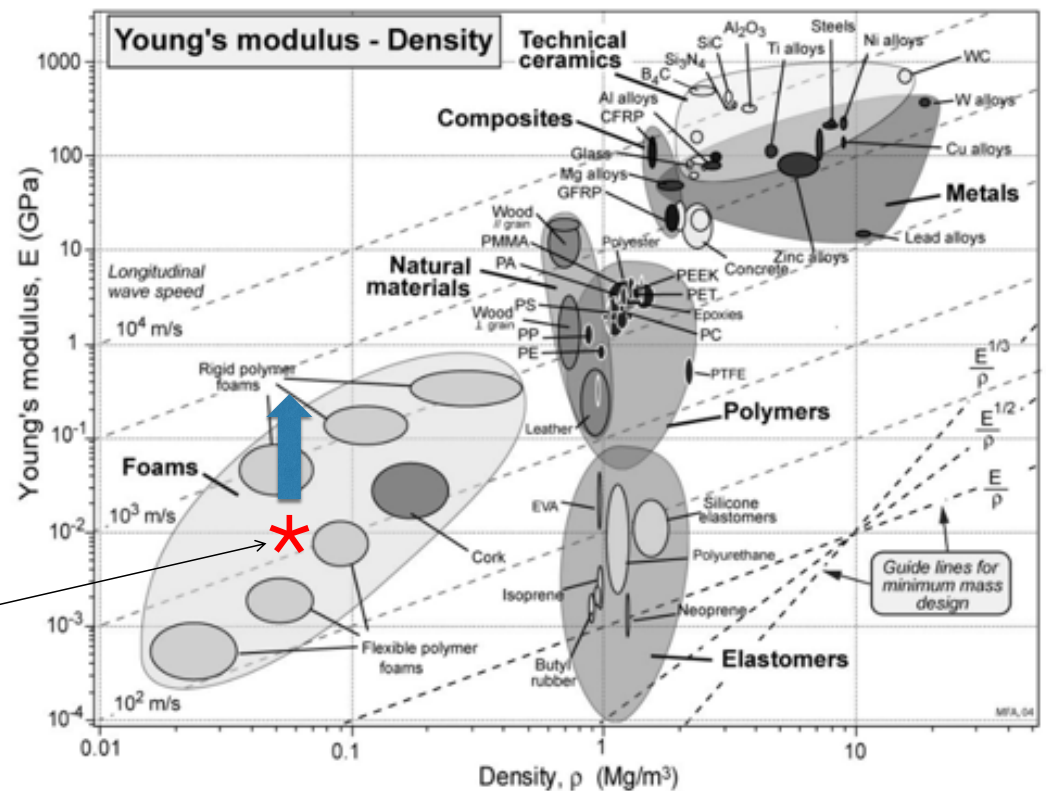
# Truss lattices

- Open cell
  - Manufacturability
  - Functional porosity
- Modeling with 1D elements
- High degree of redundancy



# Multi-material lattices

- Materials with different modulus-to-density ratios → better stiffness for same weight –or– lighter for same stiffness
- One strut / one material → easier to manufacture
- Potential for multi-functionality



# Graphical summary



$E_1 = 6.5$   
 $\gamma_1 = 0.55$

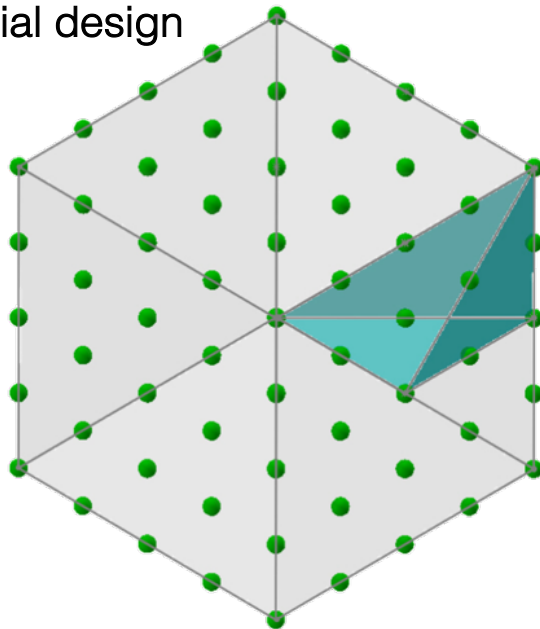


$E_2 = 5.0$   
 $\gamma_2 = 0.45$

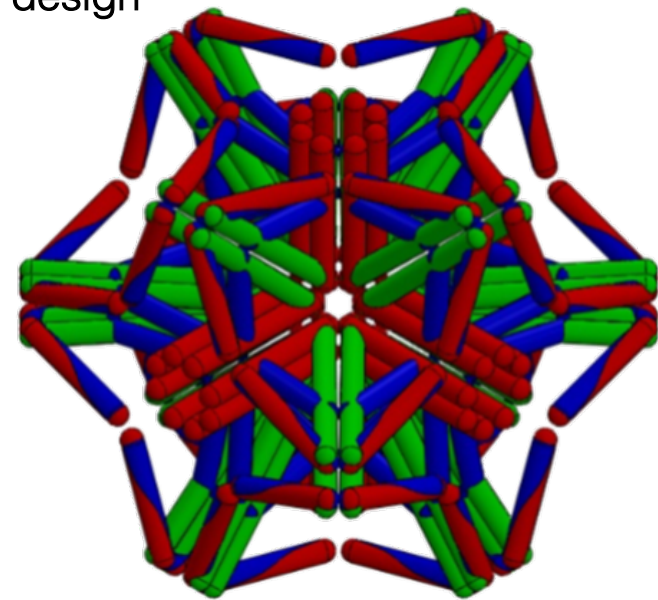


$E_3 = 4.5$   
 $\gamma_3 = 0.35$

Initial design



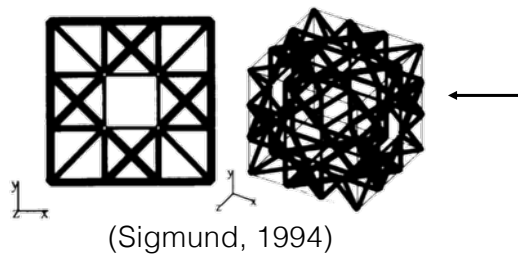
Optimal design



- Near-zero length bars made of mixture of all available materials
- Continuum mesh
- Specified material symmetries

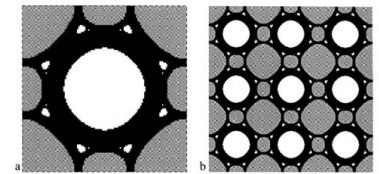
Spatial layout of struts (including removal)  
*and*  
choice of best material for each strut

# Existing approaches to lattice design



Ground  
structure TO

Density-  
based TO



(Gibianski and  
Sigmund, 2000)

Modeling accuracy

Lower

Higher

Computational cost

Lower

Higher

Design freedom

Lower

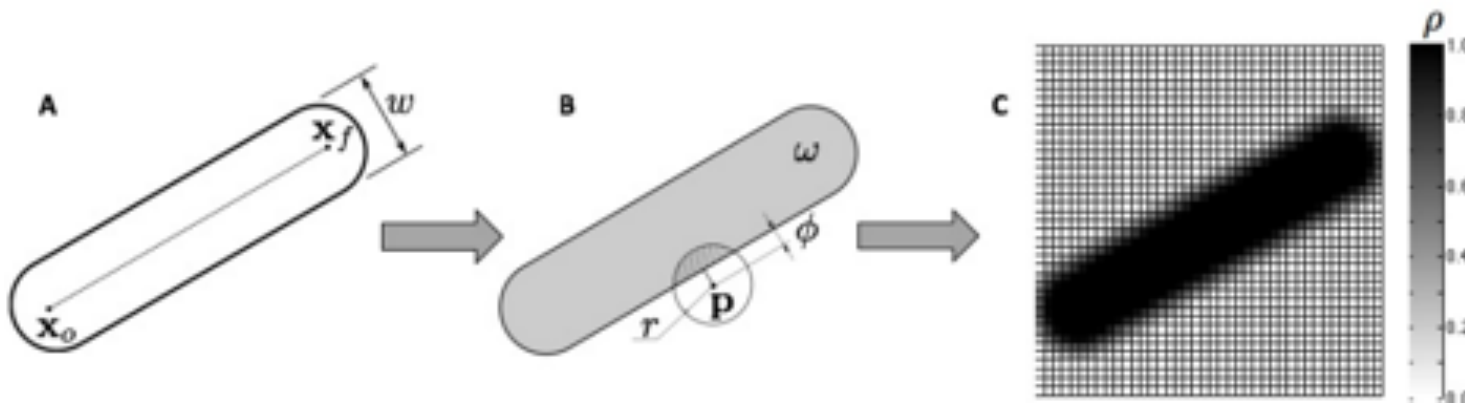
Higher

Manufacturability

Higher

Lower

# Geometry projection: the idea



Norato et al. (2004, 2015), Bell et al. (2012)

$$\rho = \frac{|\mathbf{B}_{\mathbf{p}}^r \cup \omega|}{\mathbf{B}_{\mathbf{p}}^r}$$

$$\mathbb{C}(\mathbf{z}, \mathbf{p}) = \mathbb{C}_{void} + \sum_{i=1}^{N_m} (\mathbb{C}_i - \mathbb{C}_{void}) \rho_{eff}^i(\mathbf{z}, \mathbf{p})$$

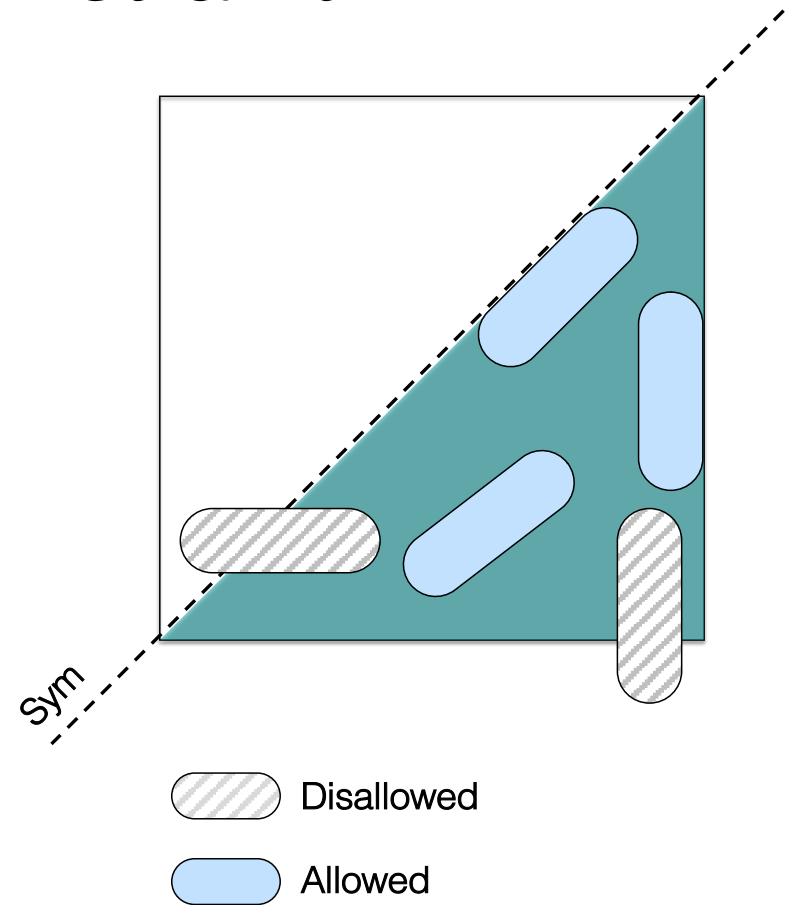
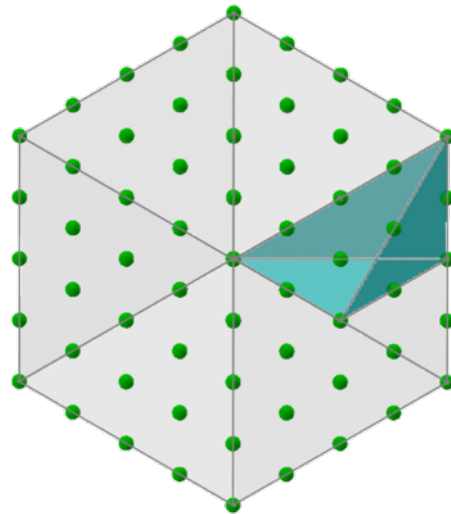
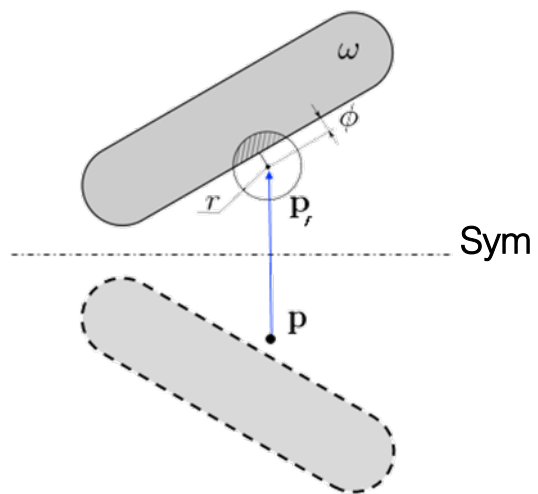
Ersatz material

Kazemi and Norato (2018)

# Comparison

	Ground structure TO	Density- based TO	Geometry Projection
Modeling accuracy	Lower	Higher	Higher
Computational cost	Lower	Higher	Higher
Design freedom	Lower	Higher	Medium
Manufacturability	Higher	Lower	Higher

# Symmetry and No-cut constraint





# Optimization problem

$$\min_{\mathbf{z}} f(\mathbf{z})$$

subject to

$$a(\mathbf{u}^{(kl)}(\mathbf{z}), \mathbf{v}) = l(\mathbf{v}, \boldsymbol{\epsilon}^{0(kl)}), \forall \mathbf{v} \in \mathcal{U}_0, \mathbf{u}^{(kl)} \in \mathcal{U}$$

$$g_w(\mathbf{z}) \leq w_f^*$$

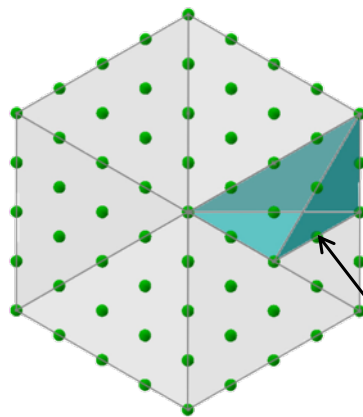
$$g_d(\mathbf{z}) \leq \epsilon_d^{(I)}$$

$$g_m(\mathbf{z}) \leq \epsilon_m^{(I)}$$

$$g_n(\mathbf{z}) \leq \epsilon_n$$

$$\mathbf{x}_{b_0}, \mathbf{x}_{b_f} \in \Omega$$

$$0.0 \leq \alpha_i^b \leq 1.0,$$



Initial design

Cubic symmetry

Bulk modulus

$$f(\mathbf{z}) \equiv -K(\mathbf{z})$$

$$K(\mathbf{z}) := \frac{1}{3}C_{1111} + \frac{2}{3}C_{1122}$$

Poisson's ratio

$$f(\mathbf{z}) \equiv \nu(\mathbf{z})$$

$$\nu(\mathbf{z}) = \frac{C_{1122}}{2(C_{1122} + C_{2121})}$$



$$E_1 = 10$$

$$\gamma_1 = 0.9$$



$$E_2 = 7.5$$

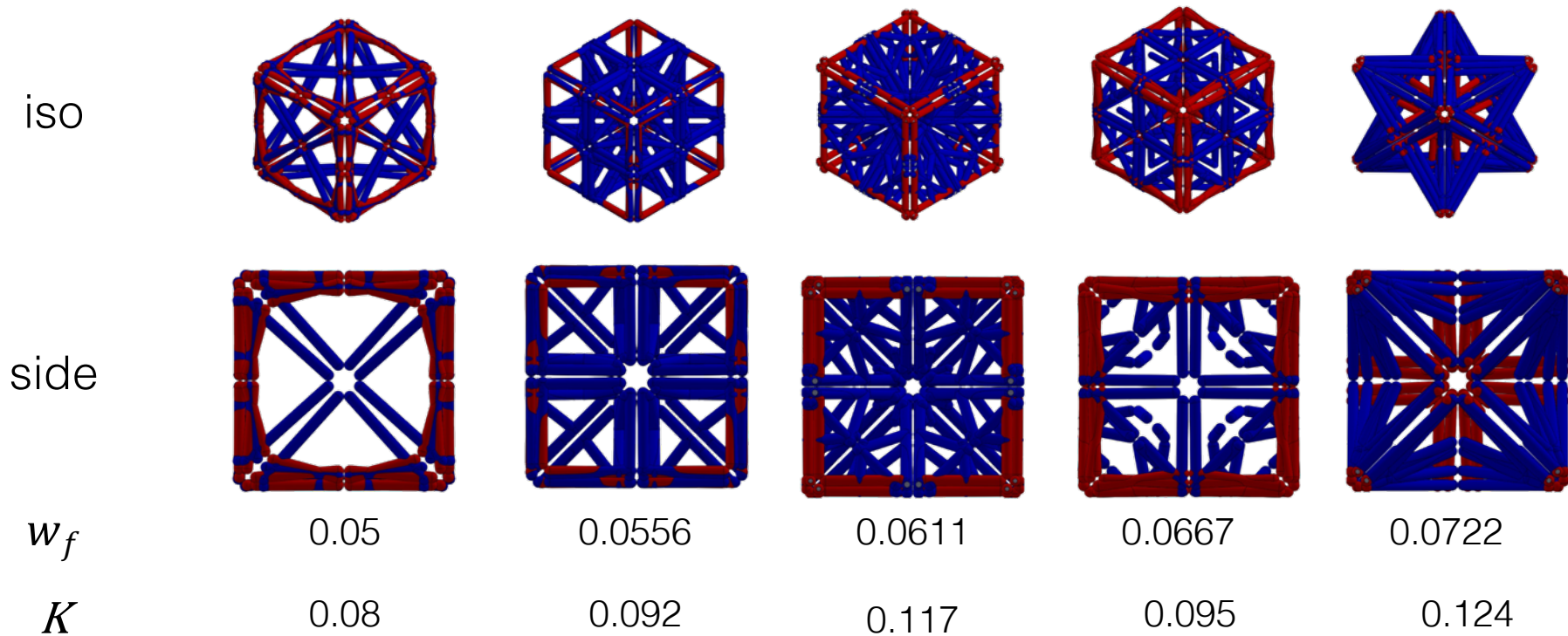
$$\gamma_2 = 0.675$$



$$E_3 = 5$$

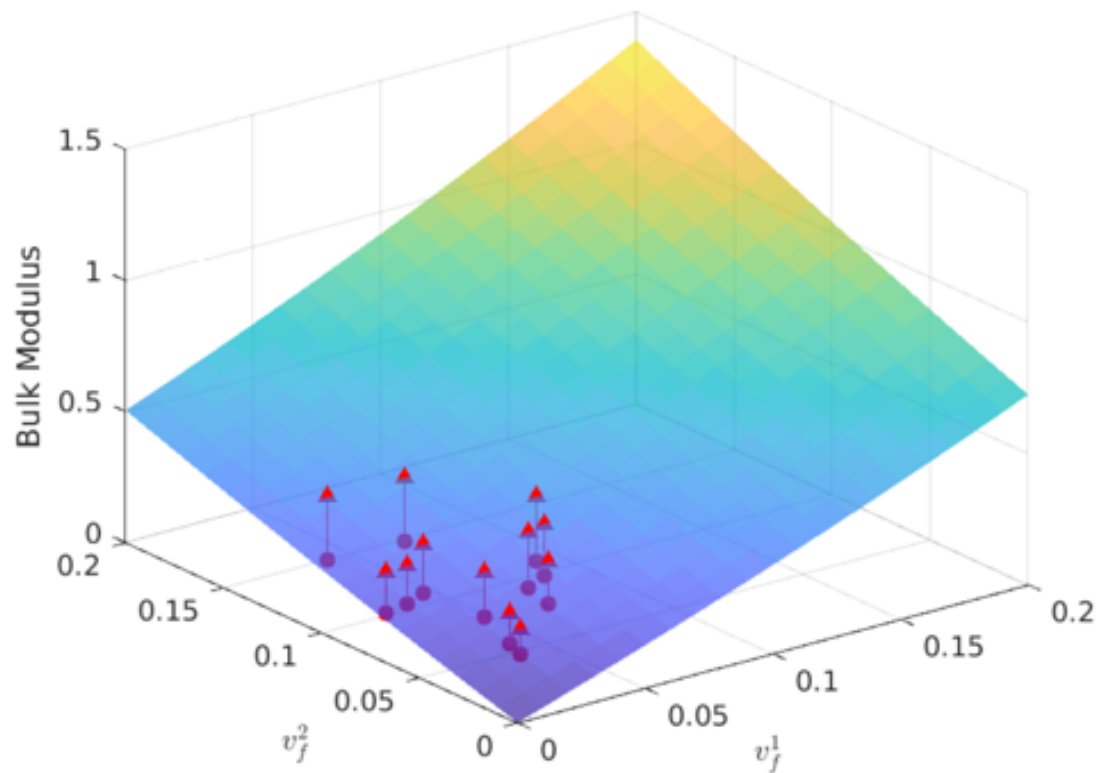
$$\gamma_3 = 0.45$$

# Bulk modulus maximization / 2 materials

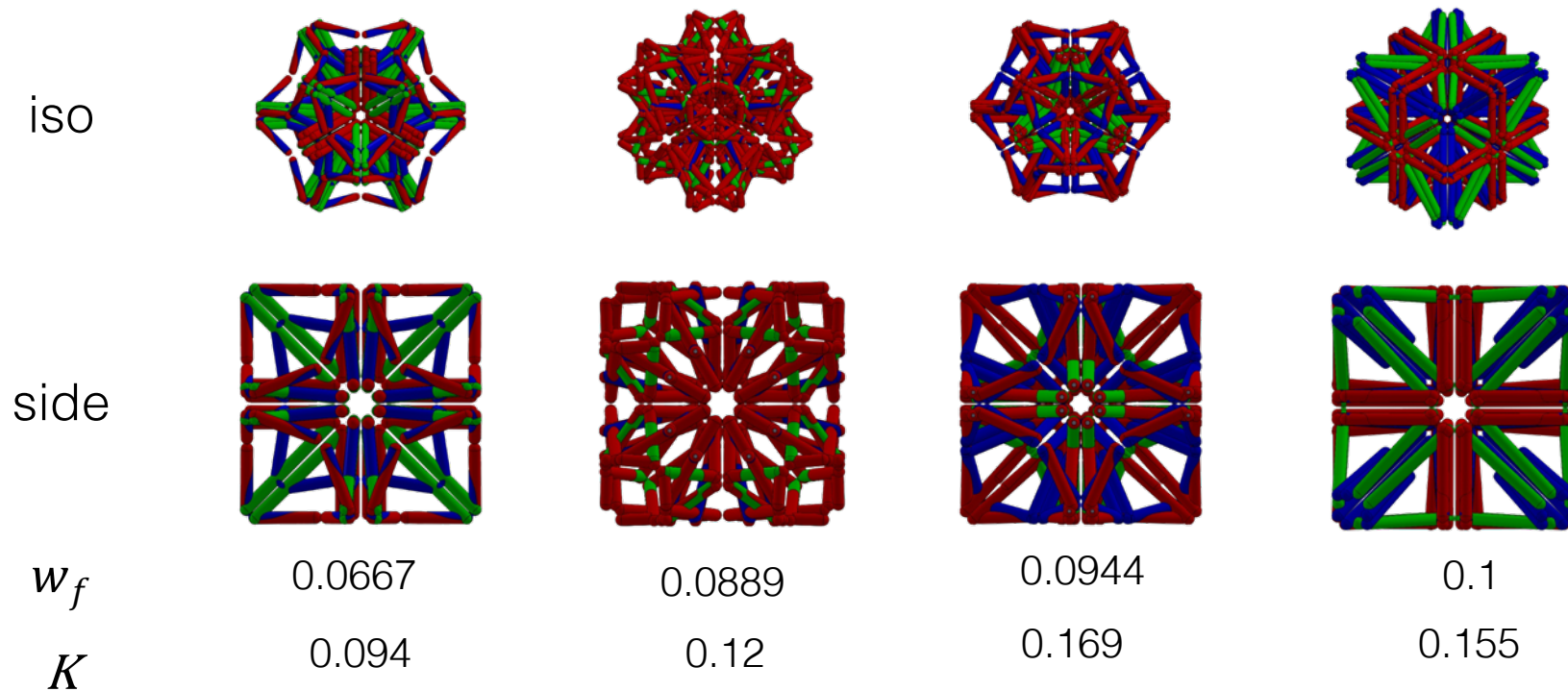


Color of struts indicates the choice of material.

# Comparison to Hashin-Shtrikman-Walpole bounds (Gibianski and Sigmund, 2000)

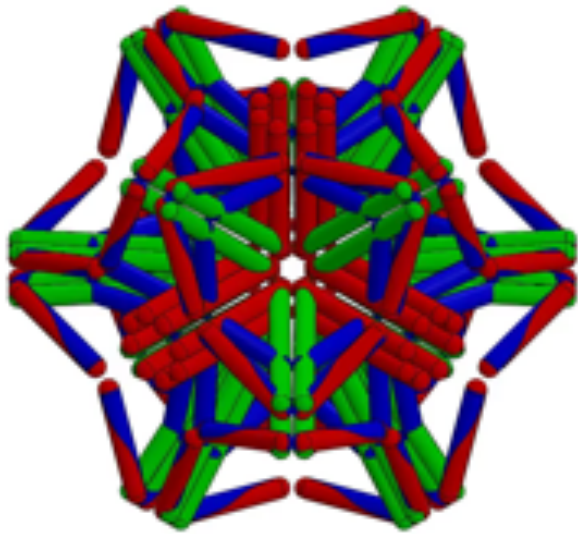


# Bulk modulus maximization / 3 materials

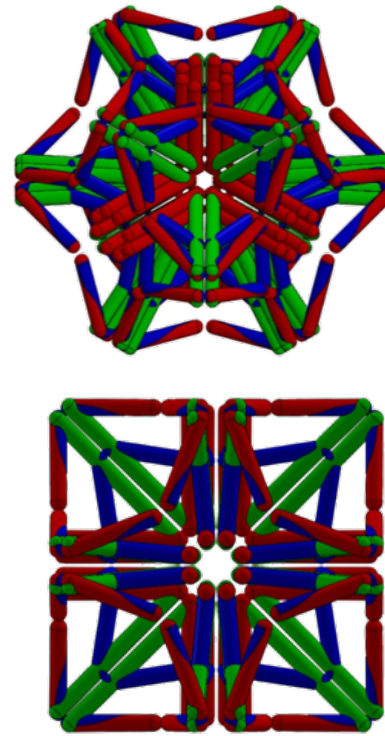


Color of struts indicates the choice of material.

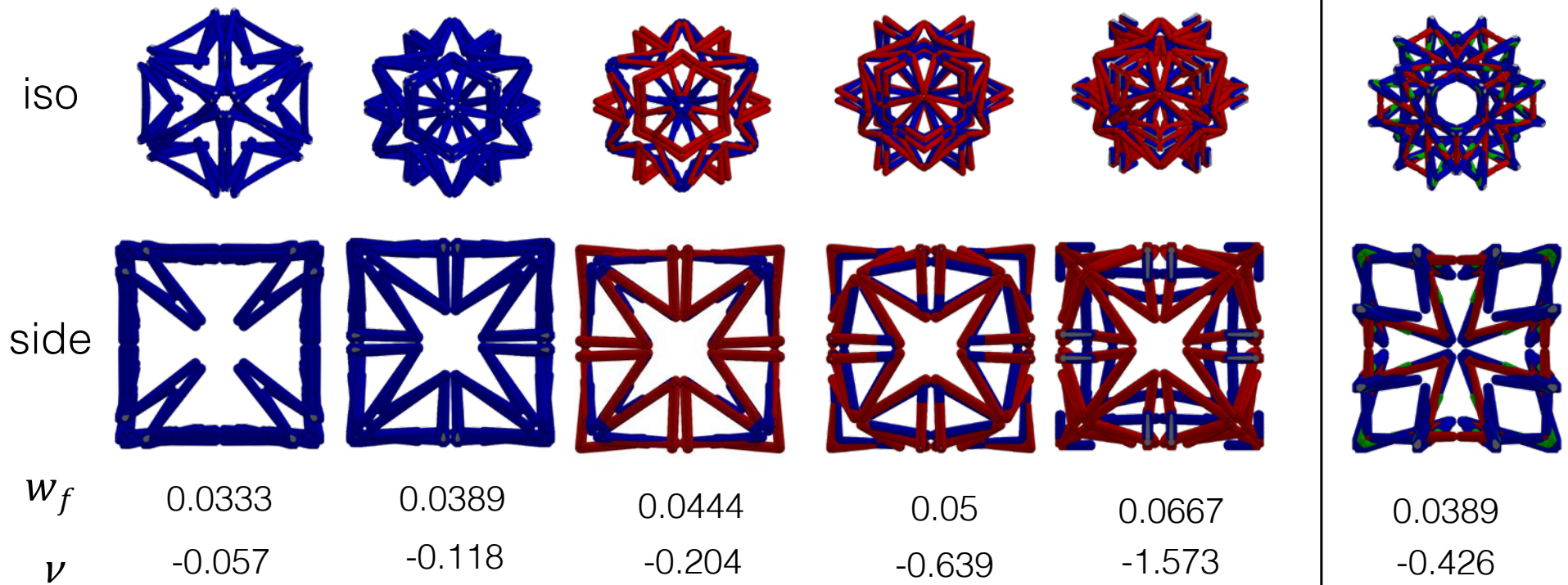
# Bulk modulus maximization / 3 materials



Bulk modulus maximization design  
for  $w_f = 0.0667$



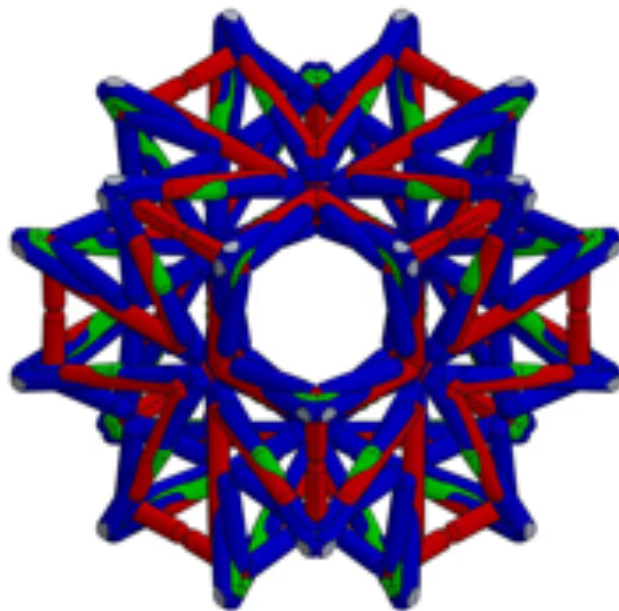
# Poisson's ratio min. / 2 and 3 materials



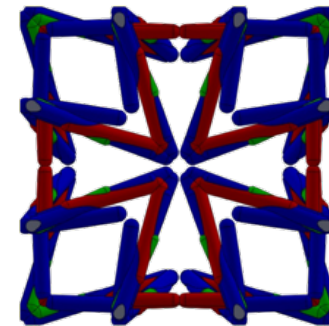
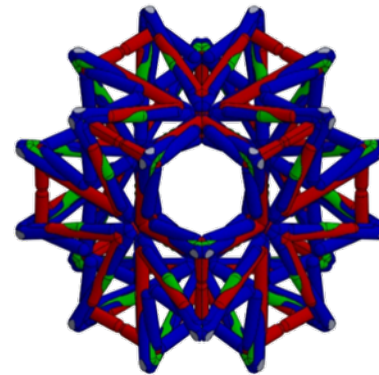
Color of struts indicates the choice of material.



# Poisson's ratio min. / 3 materials



Poisson's ratio minimization  
design for  $w_f = 0.0389$



# Epilogue

- In practice, polymeric materials for multi-material printers have similar physical densities → optimizer uses only stiffer material.
- Possibility 1: impose minimum angle constraints to prevent overlaps among struts that make manufacturing more difficult.
- Possibility 2: struts that are hollow or fiber-reinforced (work in progress)





**Thank you!**



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